

AN10951

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1805 MHz to 1880 MHz asymmetrical Doherty amplifier with
the BLF7G20LS-90P and BLF7G21LS-160P

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Application note

Document information

Info	Content
Keywords	Doherty architecture, Digital PreDistortion (DPD), IS-95, multi-carrier GSM, W-CDMA, pulse, BLF7G20LS-90P, BLF7G21LS-160P
Abstract	This application note describes the design and performance of an asymmetrical Doherty amplifier in the 1805 MHz to 1880 MHz band using the BLF7G20LS-90P and the BLF7G21LS-160P LDMOS transistors.

Revision history

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AN10951#2	20150901	Modifications <ul style="list-style-type: none">• The format of this document has been redesigned to comply with the new identity guidelines of Ampleon.• Legal texts have been adapted to the new company name where appropriate.
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1. Introduction

This application note describes the design and performance of an asymmetrical Doherty amplifier in the 1805 MHz to 1880 MHz band using the BLF7G20LS-90P and the BLF7G21LS-160P LDMOS transistors.

The asymmetrical Doherty amplifier design uses Ampleon's seventh generation push-pull LDMOS transistors BLF7G20LS-90P and BLF7G21LS-160P on a 0.51 mm (0.020") thick Rogers 4350, Printed-Circuit Board (PCB). The BLF7G20LS-90P is rated at 90 W and operates as the main amplifier for the carrier signal. The BLF7G21LS-160P is rated at 160 W and operates as the amplifier for peak signals. Both devices are internally matched at the input and output.

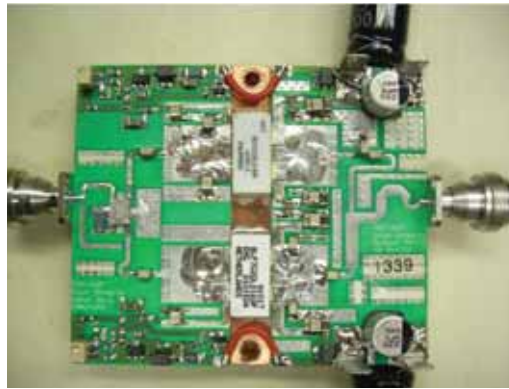


Fig 1. The assembled asymmetrical Doherty amplifier

2. Test summary

Amplifier under test: board number: 1339; date code m1001/D101504; Rogers 4350 PCB, thickness of 0.51 mm (0.020").

The amplifier was characterized under the following conditions:

- Frequency band: 1805 MHz to 1880 MHz
- Network analyzer measurements for gain (G_p), delay (t_d) and Input Return Loss (IRL) at:
 - output power (P_L) = 46 dBm
 - drain-source voltage (V_{DS}) = 28 V
 - quiescent drain current (I_{Dq}) (main amplifier) = 350 mA
 - gate-source voltage (V_{GS}) (peak amplifier) = 0.3 V
- Peak output power measurement:
 - using the standard CDMA IS-95 signal, the peak-to-average ratio (PAR) = 9.7 dB at 0.01 % probability on the CCDF to determine output power (P_L) where the PAR reaches a value of 6.7 dB at 0.01 % probability on the CCDF. This is called the 3 dB compression point. V_{DS} = 28 V, I_{Dq} (main amplifier) = 350 mA and V_{GS} (peak amplifier) = 0.3 V

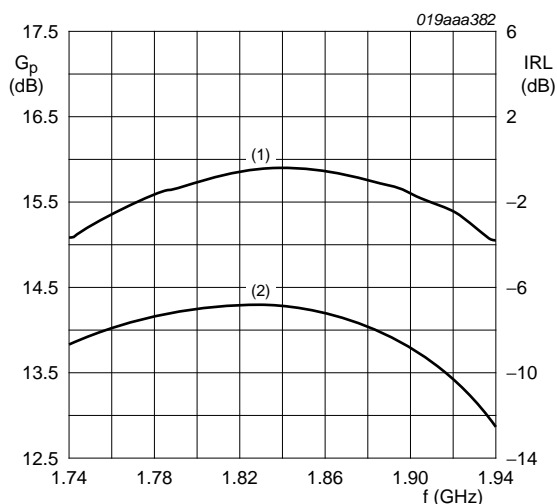
- using a pulsed signal and measuring the 1 dB and 3 dB compression points with a pulse width of 12 μ s at 10 % duty cycle: $V_{DS} = 28$ V, I_{Dq} (main amplifier) = 350 mA and V_{GS} (peak amplifier) = 0.3 V
- IS-95 measurement at $V_{DS} = 28$ V, I_{Dq} (main amplifier) = 350 mA and $V_{GS} = 0.3$ V
- 6-carrier GSM measurements using a 6-carrier GSM signal with a 4 MHz spacing, PAR = 7.5 dB at 0.01 % probability: $V_{DS} = 28$ V, I_{Dq} (main amplifier) = 350 mA and V_{GS} (peak amplifier) = 0.3 V
- Digital PreDistortion (DPD) measurements using a DPD system:
 - 2-carrier W-CDMA signal, 10 MHz spacing, peak-to-average ratio (PAR) = 7.6 dB at 0.01 % probability (total signal), $V_{DS} = 28$ V, I_{Dq} (main amplifier) = 350 mA and V_{GS} (peak amplifier) = 0.3 V
 - 2-carrier LTE signal, 10 MHz spacing, 10 MHz carrier bandwidth, peak-to-average ratio (PAR) = 7.6 dB at 0.01 % probability (total signal), $V_{DS} = 28$ V, I_{Dq} (main amplifier) = 350 mA, V_{GS} (peak amplifier) = 0.3 V

3. RF Performance

3.1 Network analyzer measurements

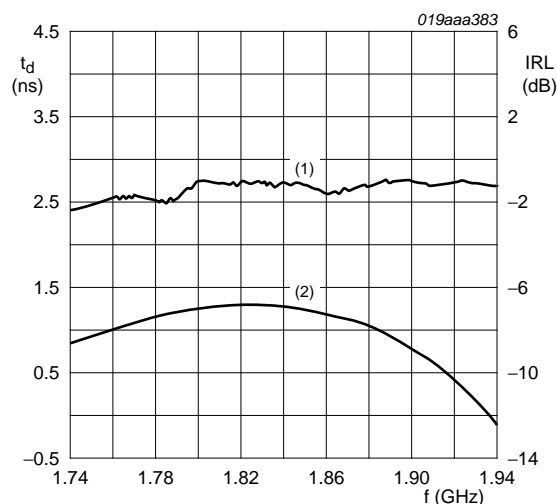
Network analyzer measurements were performed under the following conditions:

- $P_L = 46$ dBm
- $V_{DS} = 28$ V
- I_{Dq} (main amplifier) = 350 mA
- V_{GS} (peak amplifier) = 0.3 V



(1) G_p .
(2) IRL.

Fig 2. Power gain and input return loss as a function of frequency



(1) t_d .
(2) IRL.

Fig 3. Delay time and input return loss as a function of frequency

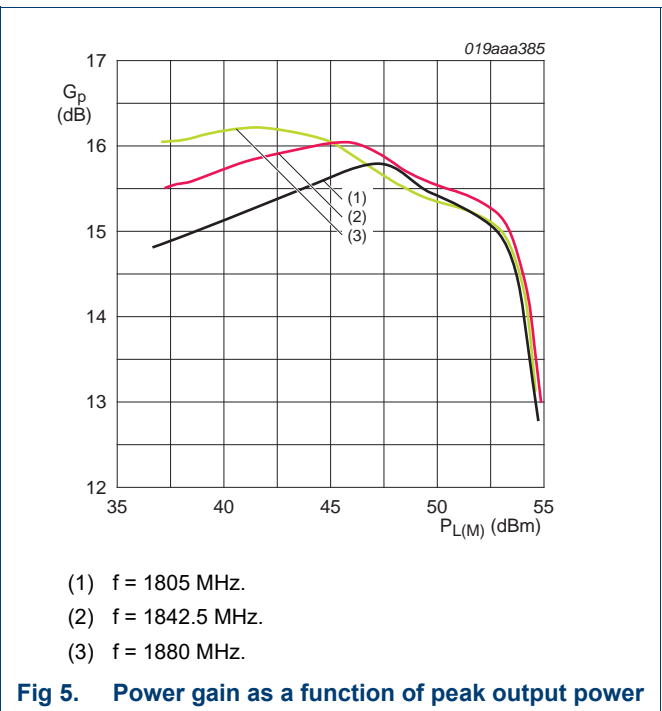
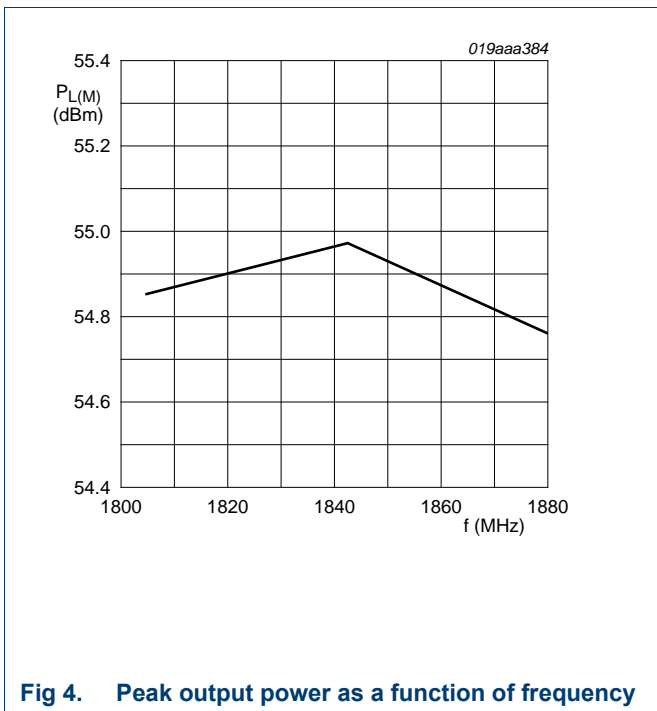
3.2 Peak output power measurements

Two methods were used to measure peak output power.

- Using a standard IS-95 signal (PAR = 9.7 dB at 0.01 % probability on the CCDF), to determine the output power when PAR reaches 6.7 dB at 0.01 % probability on the CCDF, measured as the 3 dB compression point
- Using the pulsed signal (12 μ s width and 10 % duty cycle), measuring the 1 dB and 3 dB compression points

The peak output power measurements were performed under the following conditions:

- Bias: $V_{DS} = 28$ V
- I_{Dq} (main amplifier) = 350 mA
- V_{GS} (peak amplifier) = 0.3 V

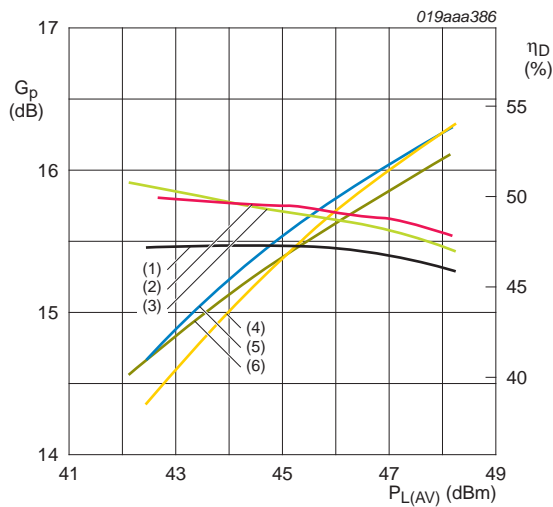


3.3 IS-95 measurements

The IS-95 measurements were performed under the following conditions:

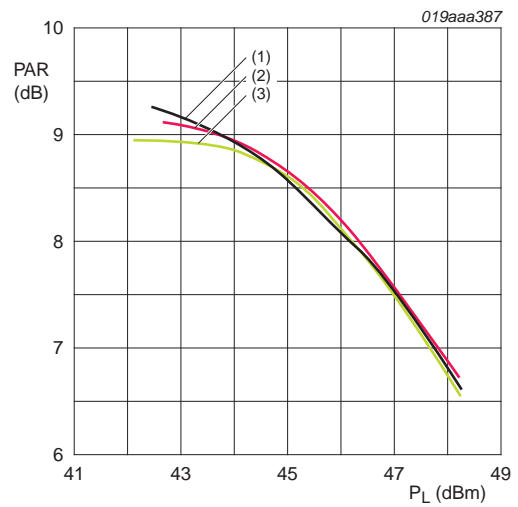
- Bias: $V_{DS} = 28\text{ V}$
- I_{Dq} (main amplifier) = 350 mA
- V_{GS} (peak amplifier) = 0.3 V

Remark: When calculating the drain efficiency, the increase in current caused by the gate temperature compensation circuit ($\cong 50\text{ mA}$) must be subtracted from the drain current value. This is approximately 50 mA.



- (1) G_p at 1805 MHz.
- (2) G_p at 1842.5 MHz.
- (3) G_p at 1880 MHz.
- (4) η_D at 1805 MHz.
- (5) η_D at 1842.5 MHz.
- (6) η_D at 1880 MHz.

Fig 6. Power gain and drain efficiency as a function of average output power, IS-95



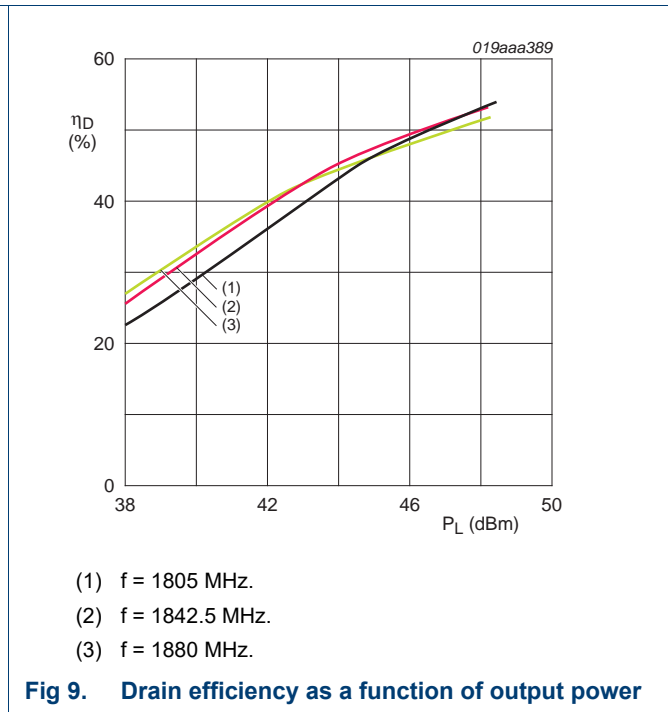
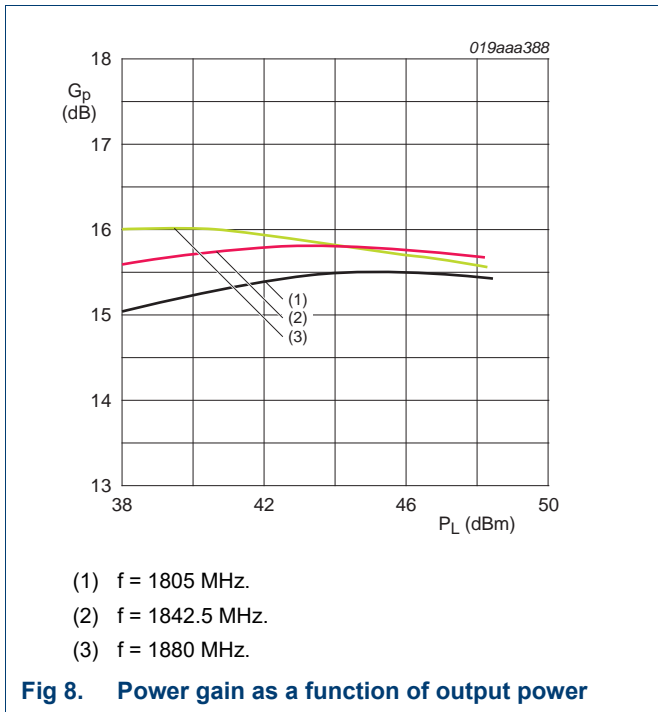
- (1) $f = 1805\text{ MHz}$.
- (2) $f = 1842.5\text{ MHz}$.
- (3) $f = 1880\text{ MHz}$.

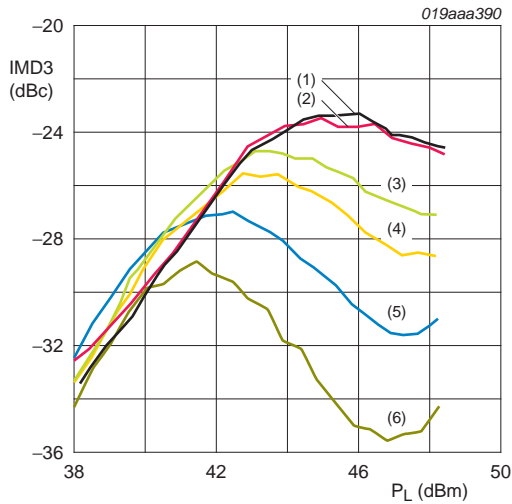
Fig 7. PAR as a function of output power

3.4 6-Carrier GSM measurements

The 6-carrier GSM measurements were performed under the following conditions:

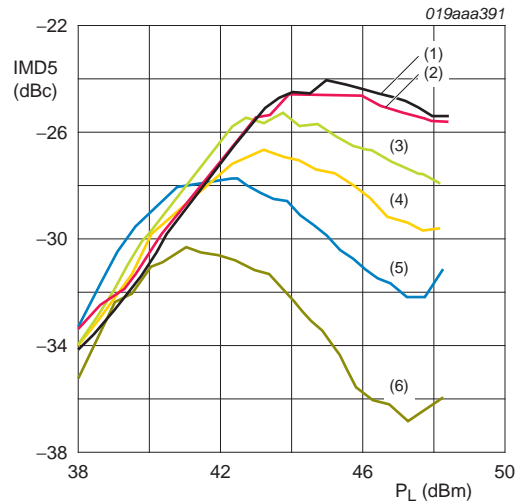
- Bias: $V_{DS} = 28\text{ V}$, I_{Dq} (main amplifier) = 350 mA and V_{GS} (peak amplifier) = 0.3 V
- Test signal: 6 carrier GSM, 4 MHz spacing, PAR = 7.5 dB at 0.01% probability
- IMD3: 4 MHz offset from the closest carrier
- IMD5: 8 MHz offset from the closest carrier





- (1) 1805 MHz IMD3 low.
- (2) 1805 MHz IMD3 high.
- (3) 1842.5 MHz IMD3 low.
- (4) 1842.5 MHz IMD3 high.
- (5) 1880 MHz IMD3 low.
- (6) 1880 MHz IMD3 high.

Fig 10. IMD3 as a function of output power



- (1) 1805 MHz IMD5 low.
- (2) 1805 MHz IMD5 high.
- (3) 1842.5 MHz IMD5 low.
- (4) 1842.5 MHz IMD5 high.
- (5) 1880 MHz IMD5 low.
- (6) 1880 MHz IMD5 high.

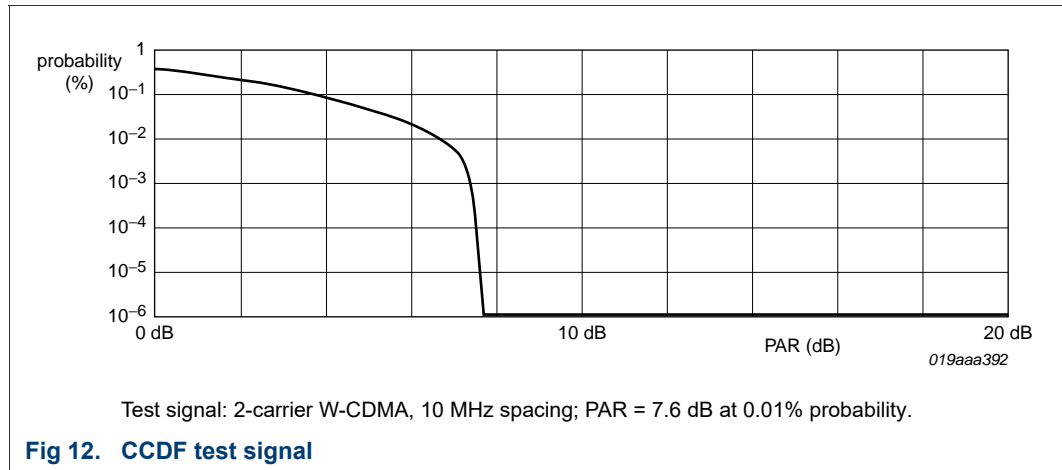
Fig 11. IMD5 as a function of output power

4. DPD Measurements

4.1 DPD measurements with 2-carrier W-CDMA

The DPD measurements were performed using a Texas Instruments DPD system under the following conditions:

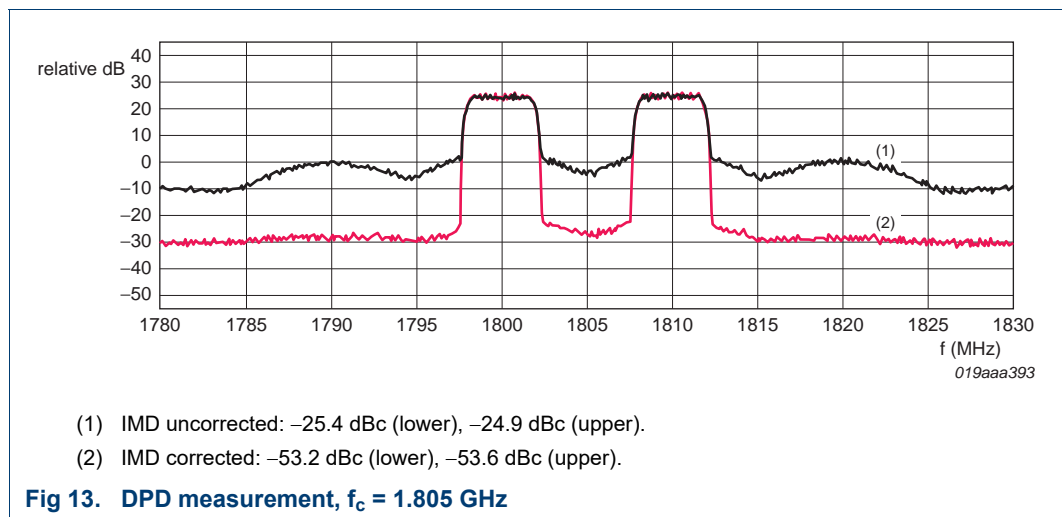
- 2-carrier W-CDMA signal, spacing: 10 MHz, peak-to-average ratio (PAR) = 7.6 dB at 0.01 % probability (total signal)
- Channel bandwidth = 3.84 MHz
- IMD: 10 MHz offset from the carrier (IBW = 3.84 MHz)
- $V_{DS} = 28$ V, I_{Dq} (main amplifier) = 350 mA, V_{GS} (peak amplifier) = 0.3 V
- IBW = 3.84 MHz



4.1.1 1.805 GHz DPD correction

The following DPD measurements were performed under the following conditions:

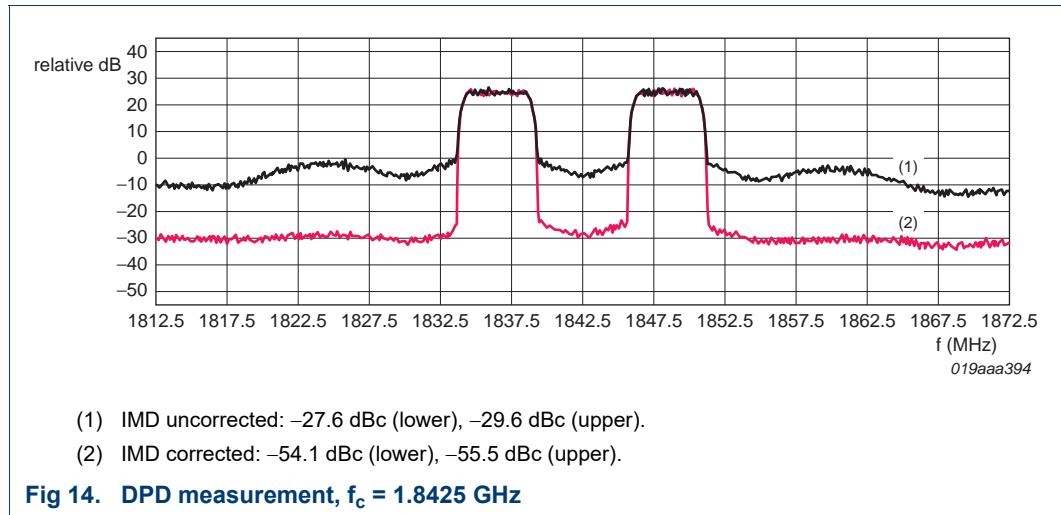
- $f_c = 1.805$ GHz
- $P_L = 46.8$ dBm
- IMD = 10 MHz offset from the carrier
- Channel bandwidth = 3.84 MHz



4.1.2 1.8425 GHz DPD correction

The following DPD measurements were performed under the following conditions:

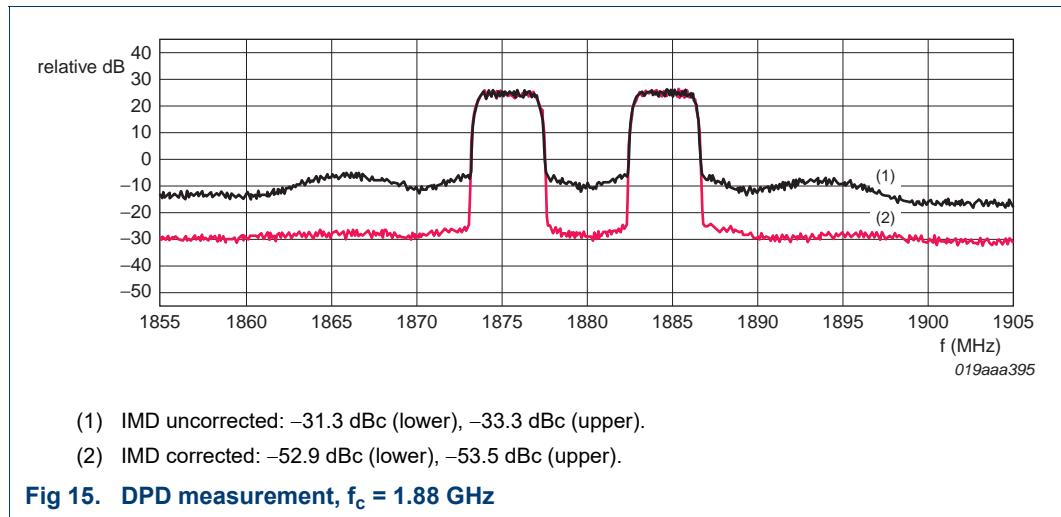
- $f_c = 1.8425$ GHz
- $P_L = 46.8$ dBm
- IMD = 10 MHz offset from the carrier
- IBW = 3.84 MHz



4.1.3 1.88 GHz DPD correction

The following DPD measurements were performed under the following conditions:

- $f_c = 1.88$ GHz
- $P_L = 46.8$ dBm
- IMD = 10 MHz offset from the carrier
- IBW = 3.84 MHz

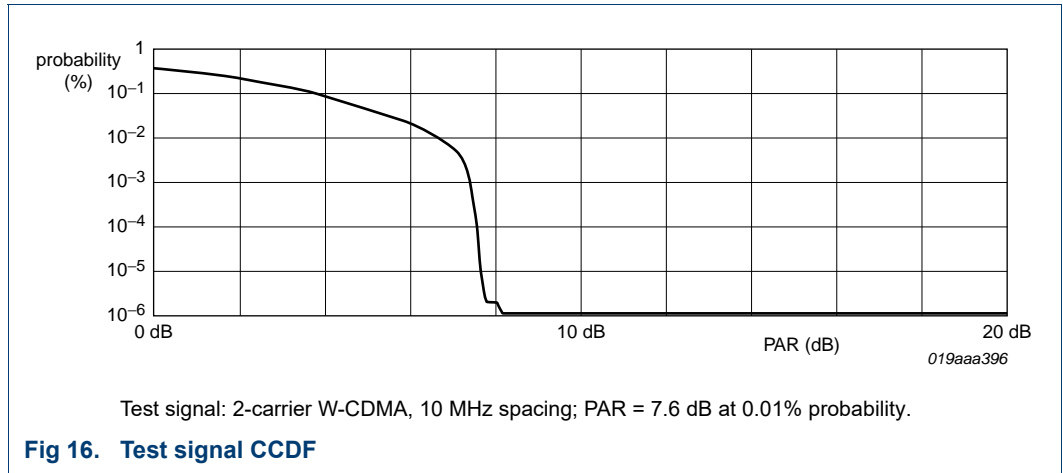


4.2 DPD measurements with 2-carrier LTE

The DPD measurements were performed using a Texas Instruments DPD system under the following conditions:

- 2-carrier LTE signal, spacing: 10 MHz, peak-to-average ratio (PAR) = 7.6 dB at 0.01 % probability (total signal)
- Channel bandwidth = 10 MHz
- ACPR: 7.5 MHz offset from the carrier (IBW = 3.84 MHz)

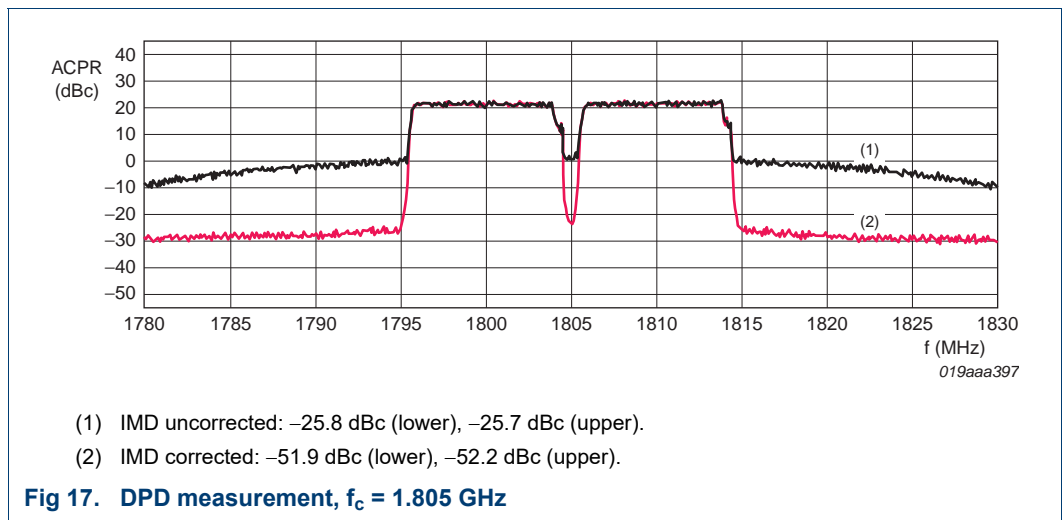
- $V_{DS} = 28\text{ V}$, I_{Dq} (main amplifier) = 500 mA, V_{GS} (peak amplifier) = 0.4 V



4.2.1 1.805 GHz DPD correction

The following DPD measurements were performed under the following conditions:

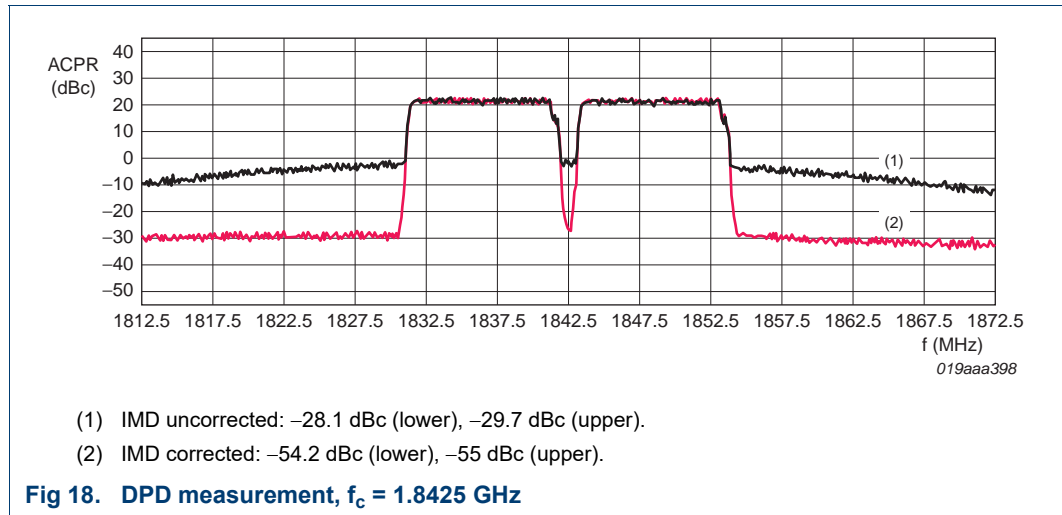
- $f_c = 1.805\text{ GHz}$
- $P_L = 46.8\text{ dBm}$
- Channel bandwidth = 10 MHz
- ACPR: 7.5 MHz offset from the carrier (IBW = 3.84 MHz)



4.2.2 1.8425 GHz DPD correction

The following DPD measurements were performed under the following conditions:

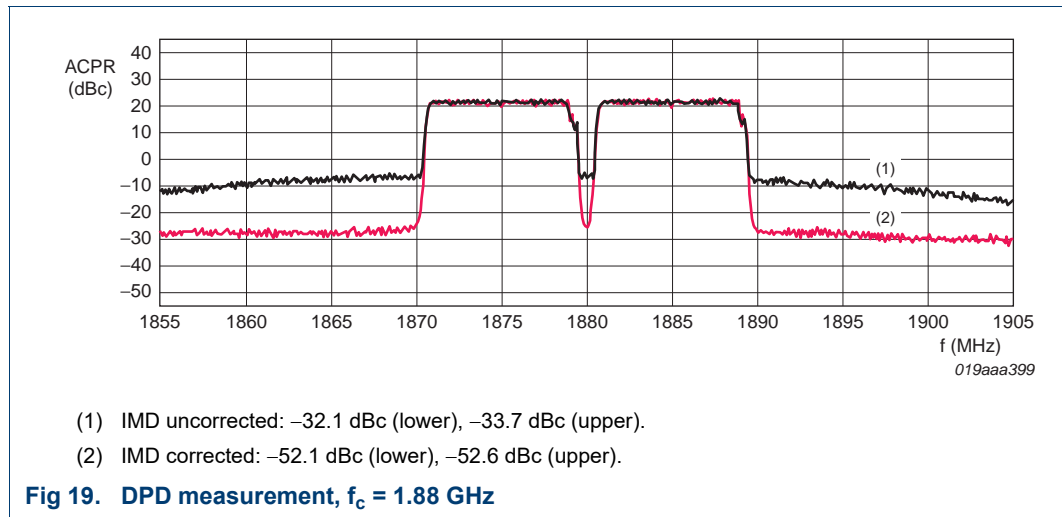
- $f_c = 1.8425\text{ GHz}$
- $P_L = 46.8\text{ dBm}$
- Channel bandwidth = 10 MHz
- ACPR: 7.5 MHz offset from the carrier (IBW = 3.84 MHz)



4.2.3 1.88 GHz DPD correction

The following DPD measurements were performed under the following conditions:

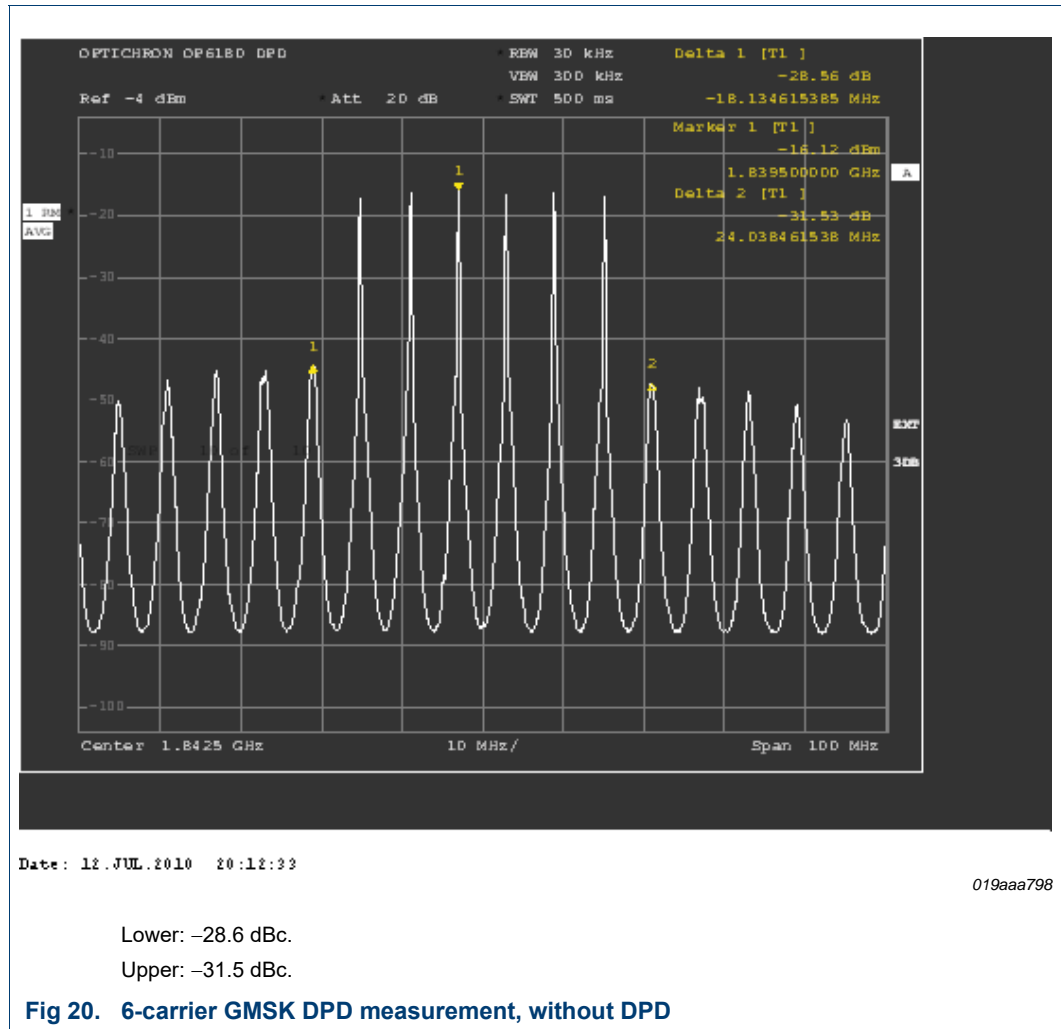
- $f_c = 1.88$ GHz
- $P_L = 46.8$ dBm
- Channel bandwidth = 10 MHz
- ACPR: 7.5 MHz offset from the carrier (IBW = 3.84 MHz)

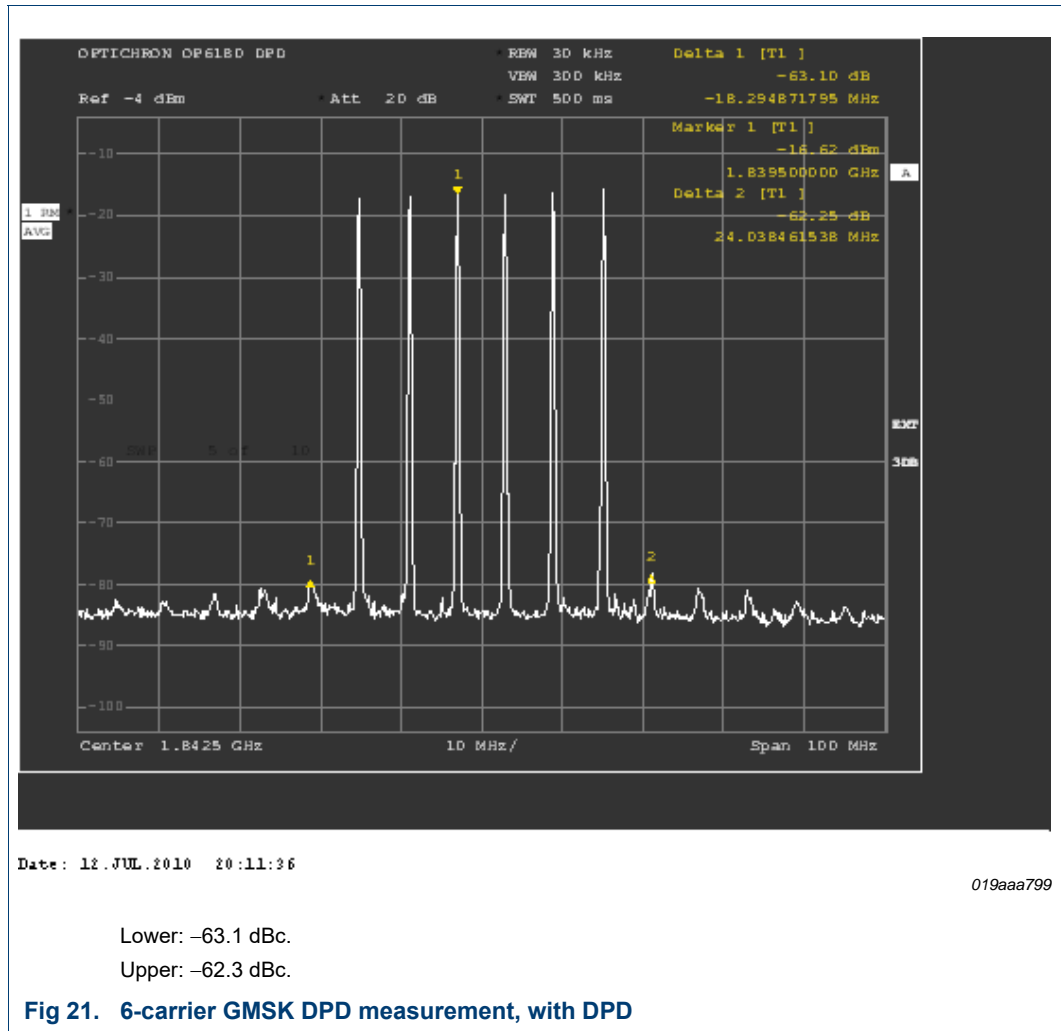


4.3 DPD measurements with 6-carrier GMSK

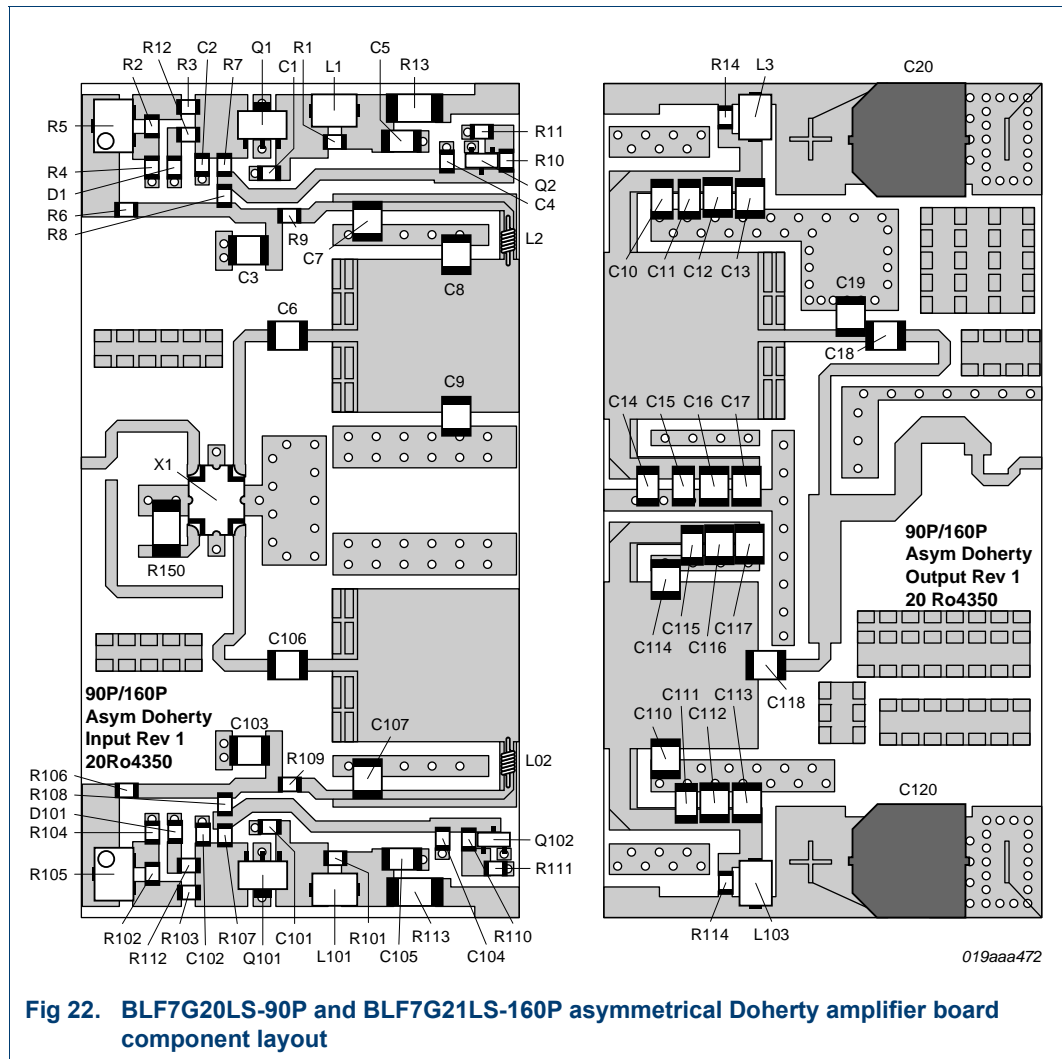
The DPD measurements were performed using an Optichron OP6180 DPD system under the following conditions:

- 6-carrier GMSK signal, spacing: 6 MHz, peak-to-average ratio (PAR) = 6.2 dB at 0.01 % probability (total signal)
- $f_c = 1.8425$ GHz
- $P_L = 47.2$ dBm





5. BLF7G20LS-90P and BLF7G21LS-160P asymmetrical Doherty amplifier board



5.1 BLF7G20LS-90P and BLF7G21LS-160P asymmetrical Doherty amplifier board components

Table 1. BLF7G20LS-90P and BLF7G21LS-160P asymmetrical Doherty amplifier board components

Designator	Description	Part identifier	Manufacturer
Input PCB	Rogers 4350; $\epsilon_r = 3.5$; thickness 0.51 mm (0.020")	-	Ohio circuits
Output PCB			
C1, C2, C4, C101, C102, C104	100 nF ceramic 0805 capacitor	S0805W104K1HRN-P4	Multicomp
C3, C5, C10, C14, C103, C105	1 μ F ceramic capacitor	GRM31CR72A105KA0	MuRata
C6, C7, C12, C16, C18, C106, C107, C112, C116, C118	30 pF ceramic chip capacitor	100B	American Technical Ceramics
C8, C9	0.9 pF capacitor	100B	American Technical Ceramics
C11, C15, C111, C115	100 nF capacitor	GRM31CR72E104KW03L	MuRata
C13, C17, C113, C117	10 μ F capacitor	100B	MuRata
C19	1.1 pF capacitor	100B	MuRata
C20, C120	220 μ F, 50 V electrolytic SMT capacitor	PCE3474CT-ND	Panasonic
C110	1.7 pF capacitor	100B	American Technical Ceramics
C114	1.6 pF capacitor	100B	American Technical Ceramics
L1, L3, L101, L103	Ferroxcube bead	2743019447	Fair Rite
L2, L102	10 nH inductor	0603CS-10NXJB	Coilcraft
Q1, Q101	78L08 voltage regulator	NJM#78L08UA-ND	NJR
Q2, Q102	2N2222 NPN transistor	MMBT2222	Fairchild
R1, R14, R101, R114	9.1 Ω resistor	CRCW08059R09FKEA	Vishay Dale
R2, R3, R102, R103, R106	430 Ω resistor	CRCW0805432RFKEA	Vishay Dale
R4	75 Ω resistor	CRCW080575R0FKEA	Vishay Dale
R104	0 Ω resistor	CRCW08050R0FKEA	Vishay Dale
R5, R105	200 Ω potentiometer	3214W-1-201E	Bourns
R6	2 k Ω resistor	CRCW08052K00FKTA	Vishay Dale
R7, R107	1.1 k Ω resistor	CRCW08051K10FKEA	Vishay Dale
R8, R108	11 k Ω resistor	CRCW080511K0FKEA	Vishay Dale
R9, R109	5.1 Ω resistor	CRCW08055R11FKEA	Vishay Dale
R10, R110	5.1 k Ω resistor	CRCW08055K10FKTA	Vishay Dale
R11, R111	910 Ω resistor	CRCW0805909RFKTA	Vishay Dale

Table 1. BLF7G20LS-90P and BLF7G21LS-160P asymmetrical Doherty amplifier board components ...continued

Designator	Description	Part identifier	Manufacturer
R12, R112	1.1 kΩ resistor	CRCW08051K10FKEA	Vishay Dale
R13, R113	499 Ω/0.5 W resistor	CRCW2010499RFKEF	Vishay Dale
R150	EMC SMT 2010 50 Ω load	-	EMC
X1	5 dB hybrid coupler	X3C19P1-05S	Anaren

6. Abbreviations

Table 2. Abbreviations

Acronym	Description
ACPR	Adjacent Channel Power Ratio
CCDF	Complementary Cumulative Distribution Function
DPD	Digital PreDistortion
GSM	Global System for Mobile communications
GMSK	Gaussian Minimum Shift Keying
IBW	Integration BandWidth
IMD	InterModulation Distortion
LDMOS	Laterally Diffused Metal-Oxide Semiconductor
LTE	Long-Term Evolution
MOSFET	Metal-Oxide Silicon Field-Effect Transistor
PAR	Peak-to-Average power Ratio
PCB	Printed-Circuit Board
W-CDMA	Wideband Code Division Multiple Access

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